

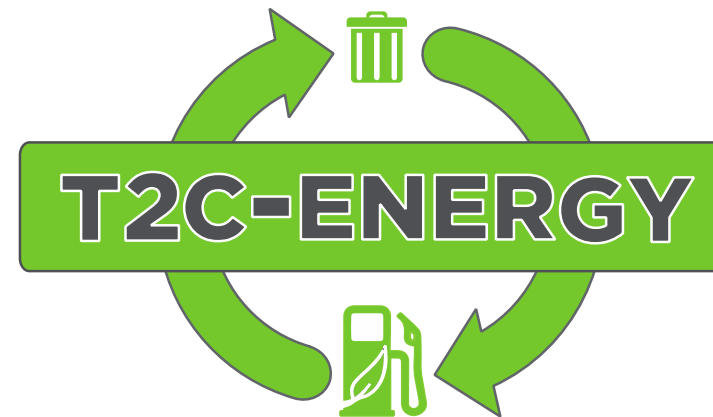
# Technologies for Upgrading Landfill Gas to a High-Quality Fuel

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John N. Kuhn

USF and T2C-Energy LLC

2023 SWANA FL Summer  
Conference



UNIVERSITY of  
**SOUTH  
FLORIDA**

# ACKNOWLEDGMENTS



Funding 2010



Winner 2012



Winner 2013



Innovation of the Year 2013



Funding 2014



Winner 2010



Funding 2014



Funding 2009



Funding 2018  
(REET)



30 Under 30 2014



Funding 2016

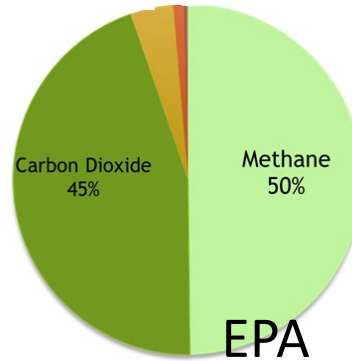


Funding 2016 (BES  
and EERE/BETO)

# THE BIG PICTURE

## Overarching Goal:

Upgrade biogas to value-added fuels and chemicals



**Biogas**  
**(~500 BTU/SCF)**

## Potential:

Diversify to value-added products, circular economy, minimize flaring

Competing options to mitigate environmental impact of biogas/landfill gas:



FLARING



ELECTRICITY



CNG/LNG



FUEL/CHEMICAL

Retail  
prices\*  
(\$/GGE)

n/a

\$1.54 (~3 cents/kWh;  
retail to grid)

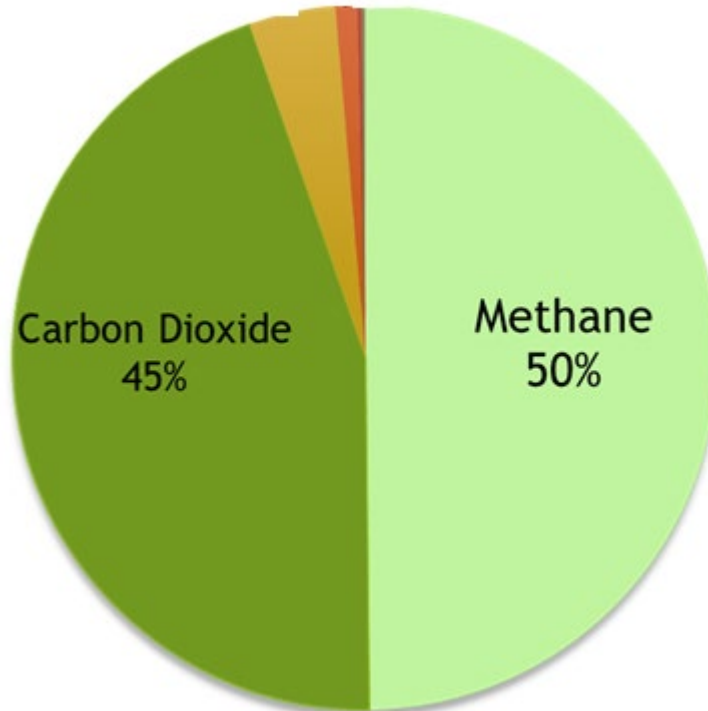
\$2.88 (CNG)  
3.63 (LNG)

\$5.17 (diesel)  
3.55 (propane)

# PROBLEM/OPPORTUNITY

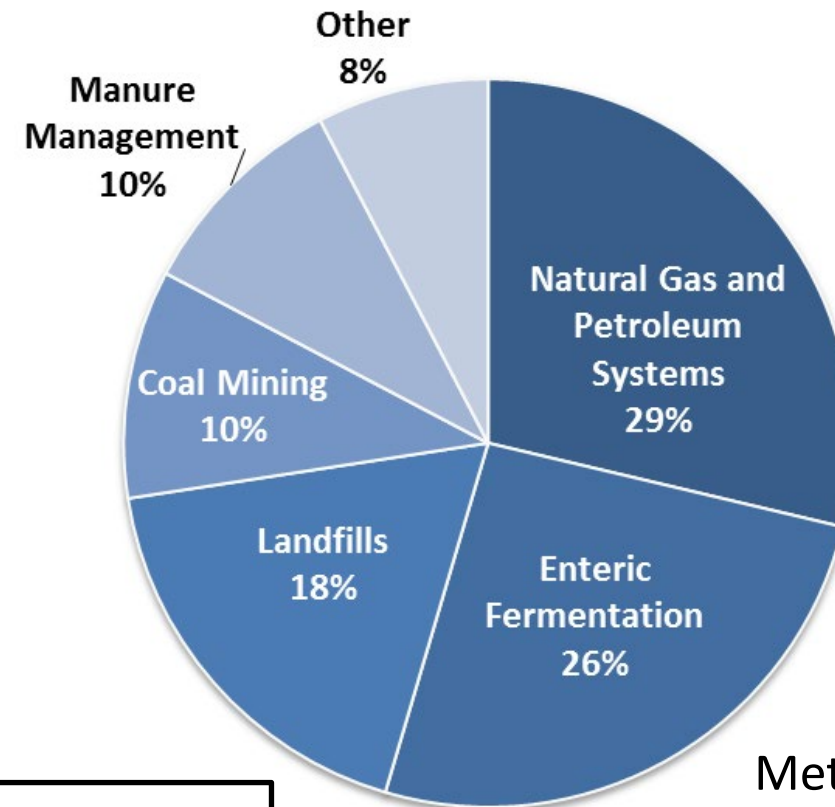
Nitrogen 4% Oxygen 4% Hydrogen 4% Halides 132 (ppm)

**Safety**



**Energy**

OFMSW (~25% of 350E6 metric tons\* / EREF\*\*)



**Environment**

Methane emissions in 2013 (EIA)

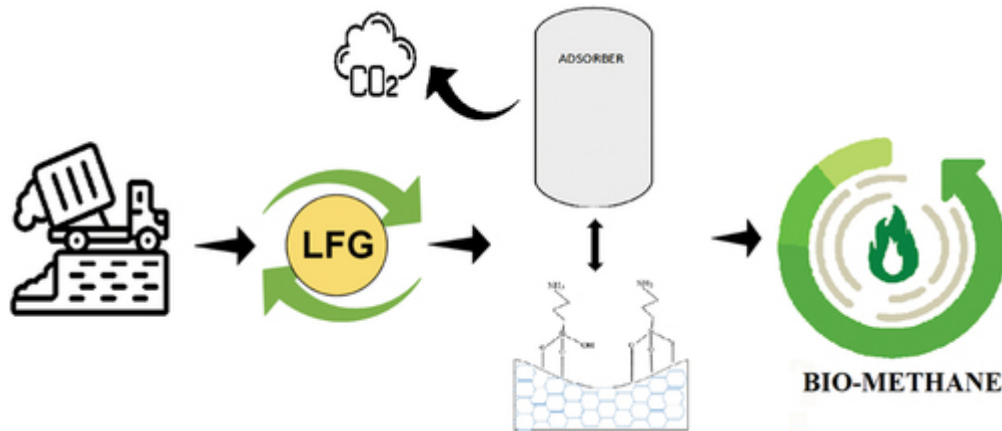
\*another 87E6 tons that is recycled and composted / \*\* 40% higher than EPA



# PROBLEM/OPPORTUNITY



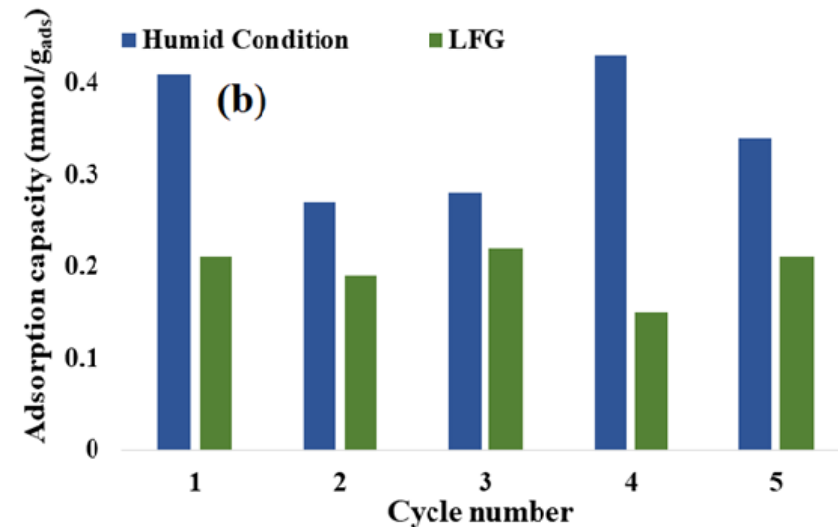
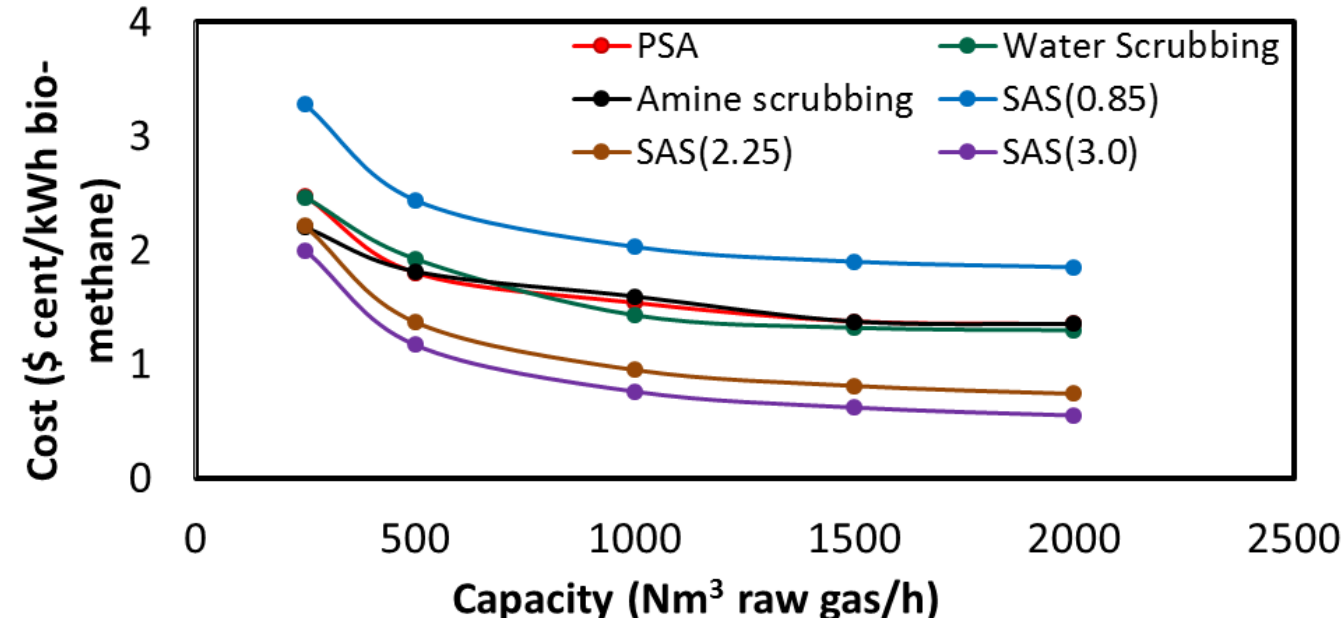
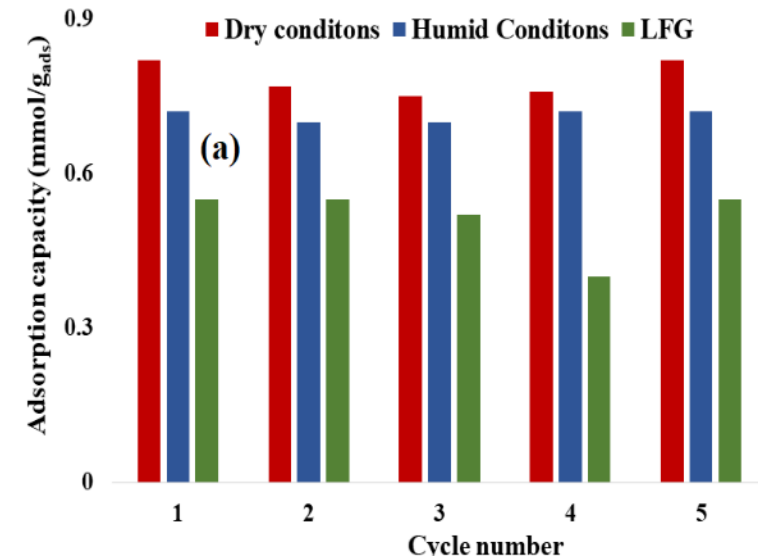
# RENEWABLE NATURAL GAS



**Table 1.** Composition of biogas used in this study.

| Compound         | Mole percent on dry basis (%) <sup>a,b</sup> |
|------------------|--|
| CH <sub>4</sub>  | 56.7   |
| CO <sub>2</sub>  | 40.5   |
| N <sub>2</sub>   | 2.4  |
| O <sub>2</sub>   | 0.4  |
| H <sub>2</sub> S | 68 (ppm)                                     |
| CO               | 6 (ppm)                                      |
| Siloxanes        | 4 (ppm)                                      |
| Halides          | 3 (ppm)                                      |

b – LFG is water-saturated  
a – Unless stated otherwise.



(PSA, Water scrubbing, and amine scrubbing data from Peterson & Wellinger, 2009)

# NEED FOR HYDROCARBON FUELS

## Plastics \*

- 8300 million metric tons plastics produced to date
- 6300 million metric tons plastics discarded as waste to date
- Of waste, 9% recycled, 12% incinerated, and 79% landfilled
- 12,000 million metric tons anticipated by 2050 (landfilled or in environment)
- Only 4 million metric tons of bio-based biodegradable
- ~13 % of U.S. MSW is plastics in 2013 (before recycling)\*\*

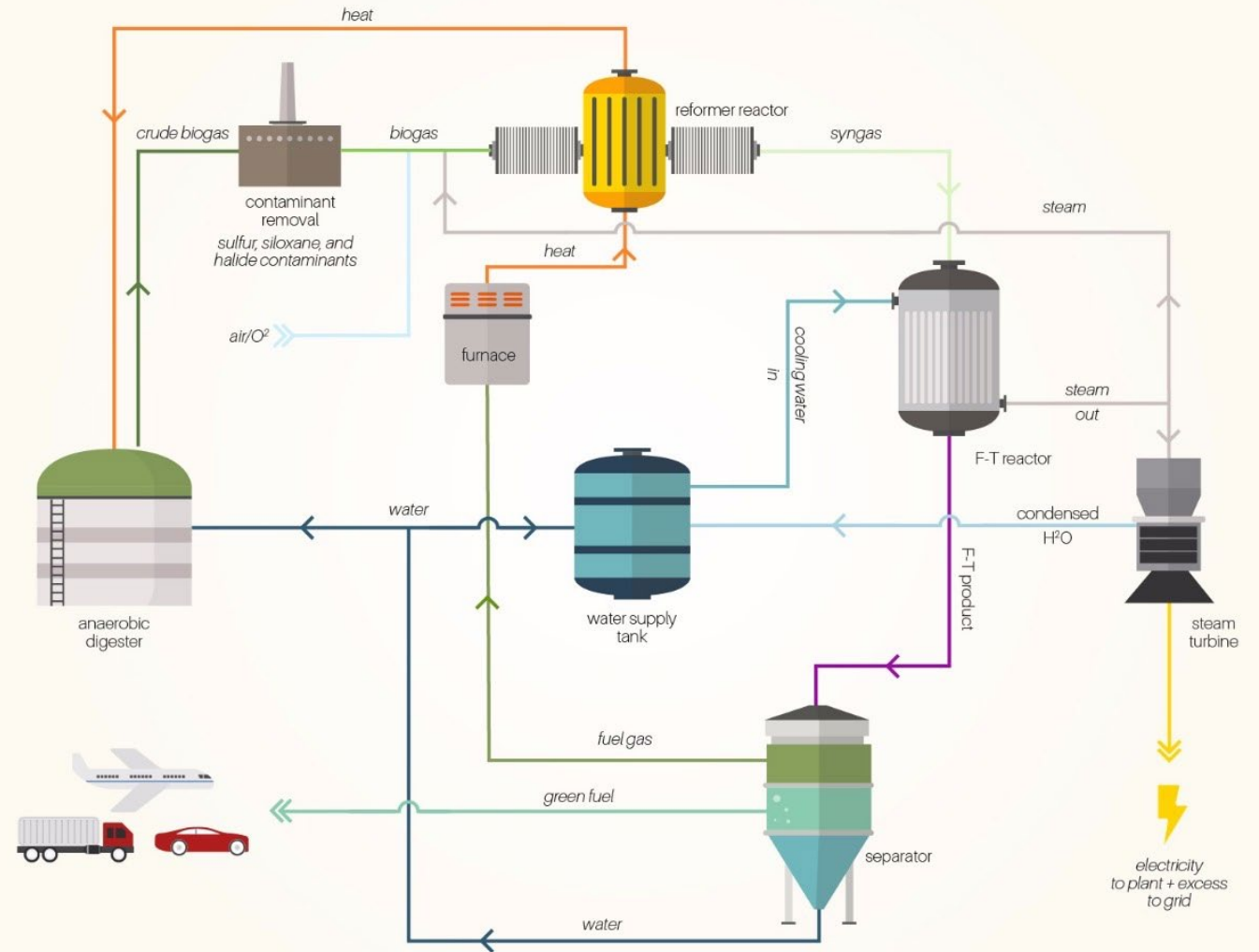
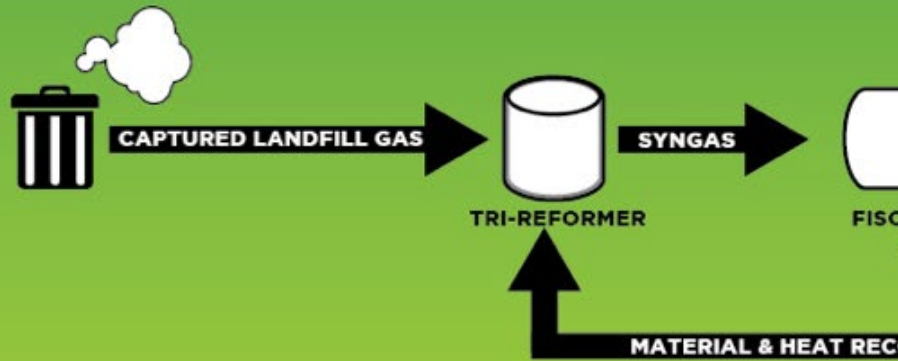
## Energy-Dense Liquid Hydrocarbon Fuels (i.e., Diesel)

- 100 million bbl crude oil used worldwide per day (~25% in U.S.)
- Equates to 4500 million metric tons per year
- Need for diesel expected to increase
- Waste industry represents 4% of US diesel consumption
- Diesel and jet fuel harder to replace than gasoline

# TRIFTS™ PROCESS OVERVIEW\*

7,500 gallons/day of fuel

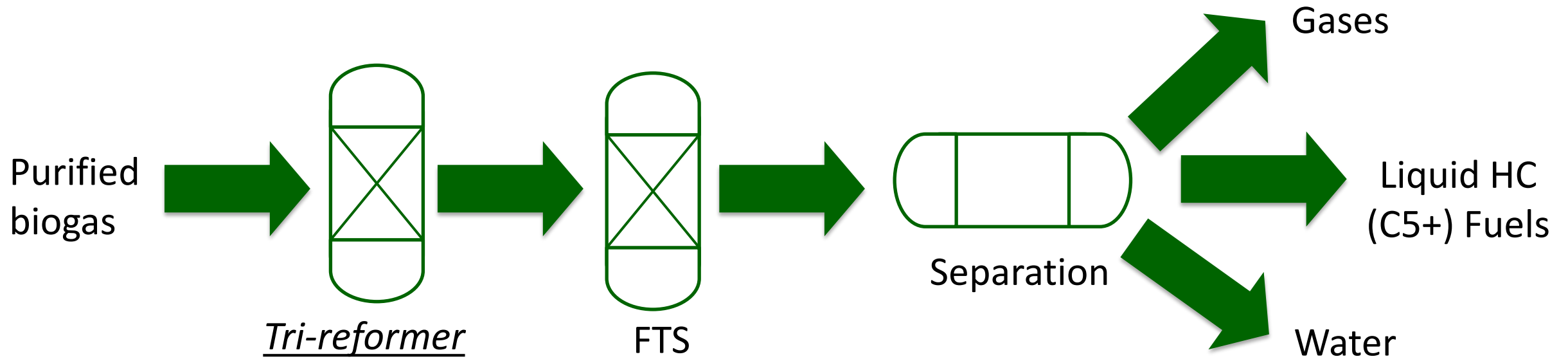
## HOW OUR PROCESS WORKS



\* Patent approved

[www.t2cenergy.com](http://www.t2cenergy.com)

# TRIFTS PROCESS OVERVIEW\*

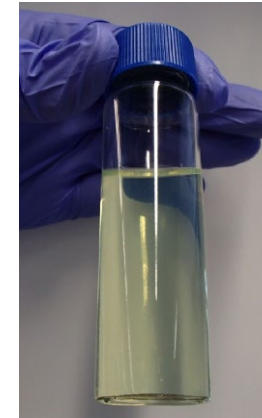


## Process simplification:

- CO<sub>2</sub> not removed from feed
- No WGS or hydrocracker (No H<sub>2</sub> needed)
- No/minimal distillation
- No air separation

- Drop-in fuel
- Low sulfur
- Low aromatics

Catalysts are key



\* Neglecting purification train here



# LAB/BENCH SCALE TRIFTS™ UNIT



## Microreactor

- 100 mg ref. catalyst
- < 100 SCCM
- Powder catalyst
- Low Pressure
- No MTL/HTL

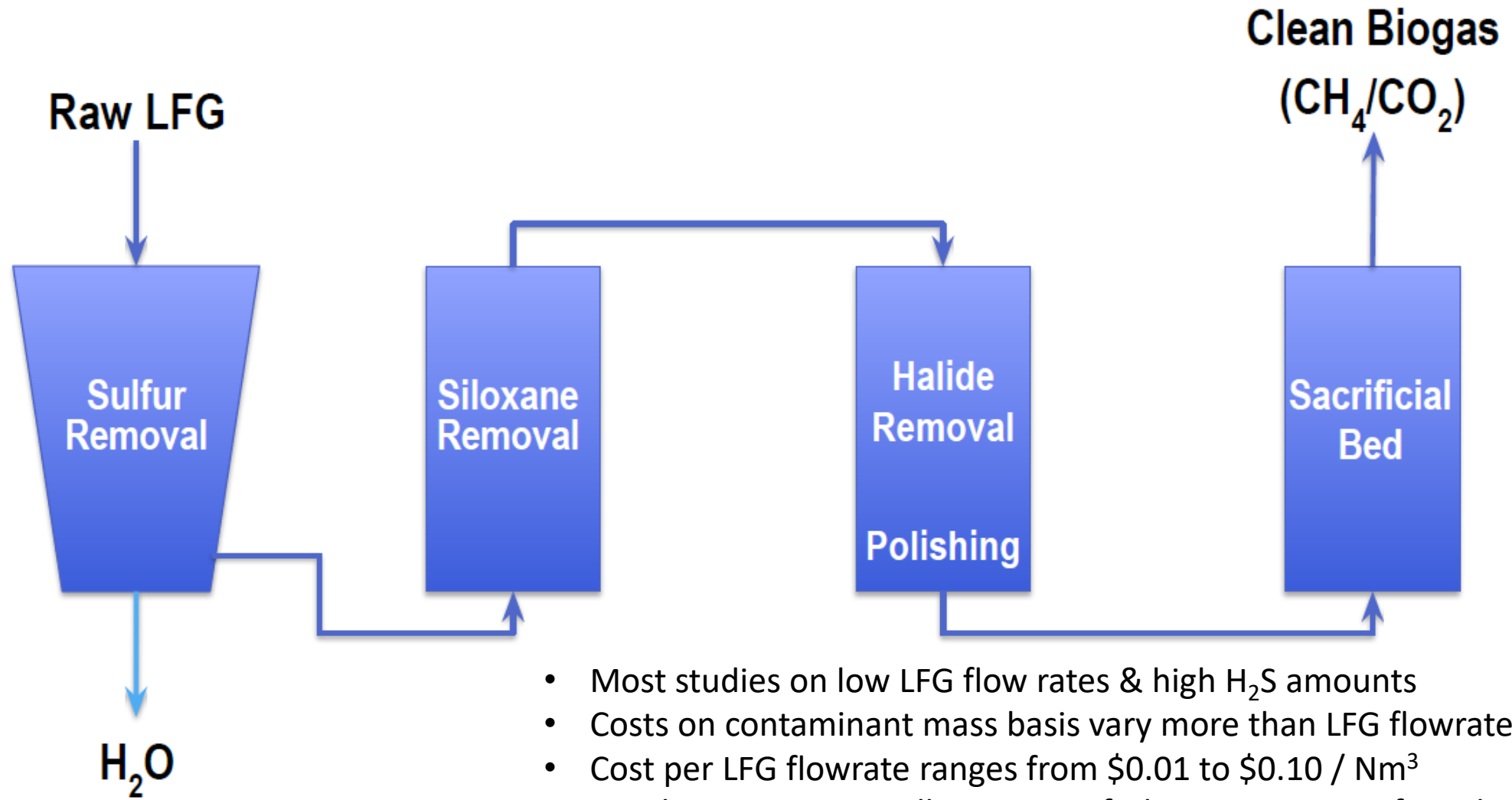
## Bench Scale\*

- ~ 3 g ref. catalyst
  - 1-3 sLPM
- Pellet catalyst
- Pressure < 30 bar
  - MTL/HTL ?





# PURIFICATION TRAIN



- Most studies on low LFG flow rates & high H<sub>2</sub>S amounts
- Costs on contaminant mass basis vary more than LFG flowrate
- Cost per LFG flowrate ranges from \$0.01 to \$0.10 / Nm<sup>3</sup>
- Need to separate small amounts of siloxanes can significantly add to costs

# LFG CONTAMINANTS

## Siloxanes

|  |     |            |
|--|-----|------------|
| Hexamethyldisiloxane[L2]: (C <sub>6</sub> H <sub>18</sub> OSi <sub>2</sub> )                         | 162 | 0.38-5.0   |
| Octamethyltrisiloxane[L3]: (C <sub>8</sub> H <sub>24</sub> O <sub>2</sub> Si <sub>3</sub> )          | 236 | 0.23-0.05  |
| Decamethyltetrasiloxane[L4]: (C <sub>10</sub> H <sub>30</sub> O <sub>3</sub> Si <sub>4</sub> )       | 310 | 0.005-0.1  |
| Hexamethylcyclotrisiloxane [D3]: (C <sub>6</sub> H <sub>18</sub> O <sub>3</sub> Si <sub>3</sub> )    | 222 | 0.01-0.84  |
| Octamethylcyclotetrasiloxane [D4]: (C <sub>8</sub> H <sub>28</sub> O <sub>4</sub> Si <sub>4</sub> )  | 297 | 1.083-15.0 |
| Decamethylcyclopentasiloxane [D5]: (C <sub>10</sub> H <sub>30</sub> O <sub>5</sub> Si <sub>5</sub> ) | 371 | 0.40-1.135 |

## Sulfur

|                                      |      |          |
|--------------------------------------|------|----------|
| Hydrogen Sulfide: (H <sub>2</sub> S) | 34.1 | 99.9-280 |
| Methanethiol: (CH <sub>3</sub> S)    | 48.1 | 0.56     |

## Halides

|  |       |                |
|--|-------|----------------|
| CarbonTetrachloride (CCl <sub>4</sub> )              | 154   | 41.5-124.3 ppb |
| Chloroform (CHCl <sub>3</sub> )                      | 113   | 78.6-183.9 ppb |
| Trichloroethene (C <sub>2</sub> HCl <sub>3</sub> )   | 131   | 0.9-2.6        |
| Tetrachloroethene: (C <sub>2</sub> Cl <sub>4</sub> ) | 165.8 | 0.14-0.30      |
| Chlorobenzene: (C <sub>6</sub> H <sub>5</sub> Cl)    | 112.6 | 0.22           |

## Mercury

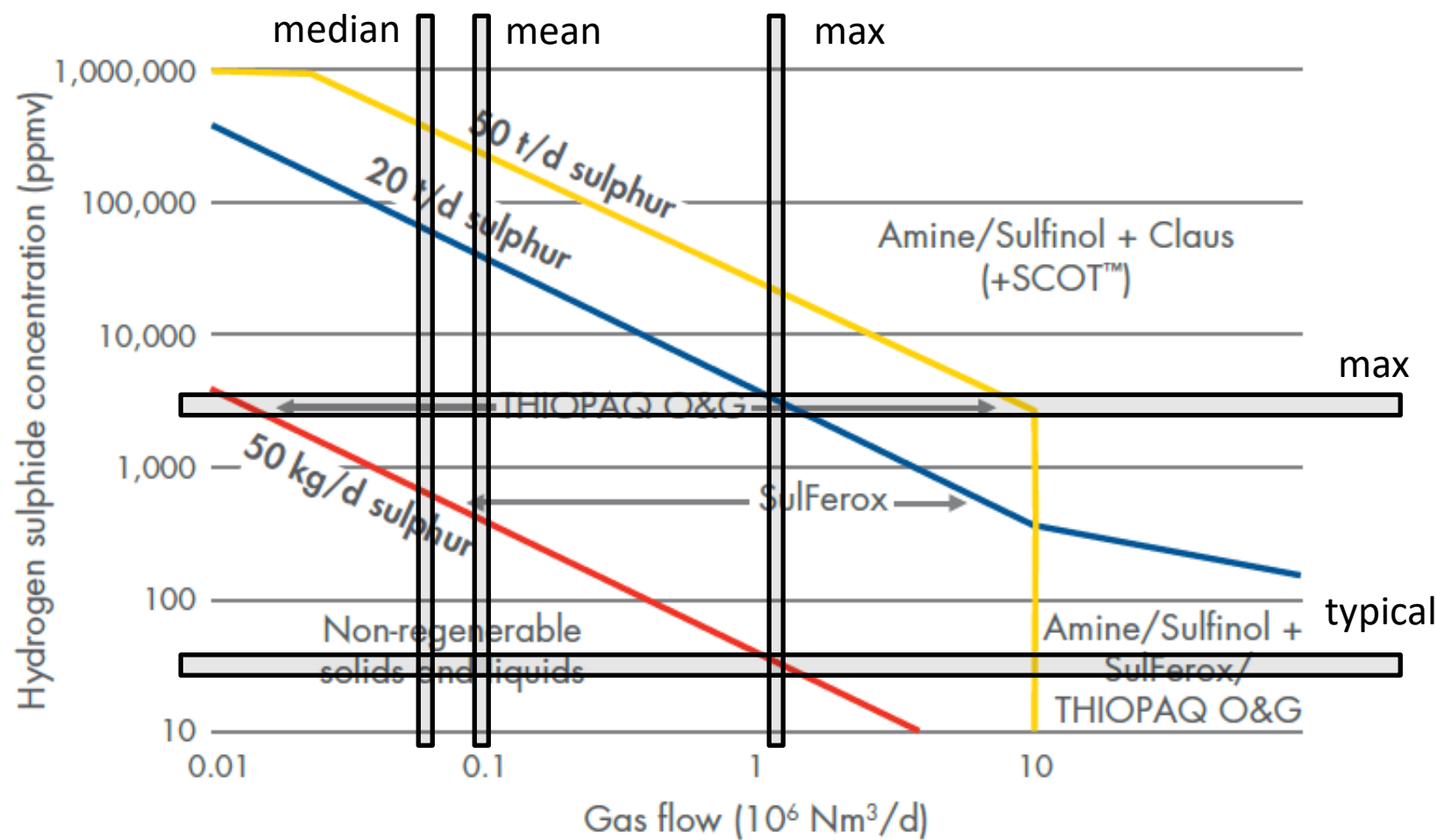
|  |     |                       |
|--|-----|-----------------------|
| MonomethylMercury (CH <sub>3</sub> Hg) | 216 | 1-47ng/m <sup>3</sup> |
|--|-----|-----------------------|

## NMOCs

|  |       |           |
|--|-------|-----------|
| Isopropyltoluene: (C <sub>10</sub> H <sub>14</sub> ) | 134.2 | 48.8-73.6 |
| α-pinene: (C <sub>10</sub> H <sub>16</sub> )         | 136.2 | 4.4-85.3  |
| Camphene: (C <sub>10</sub> H <sub>16</sub> )         | 136.2 | 1.5-5.4   |
| Limonene: (C <sub>10</sub> H <sub>16</sub> )         | 136.2 | 15.8-52.9 |
| Terpinene: (C <sub>10</sub> H <sub>16</sub> )        | 136.2 | 3.4-10.7  |
| Octane: (C <sub>8</sub> H <sub>18</sub> )            | 114.2 | 3.5-6.0   |
| Nonane: (C <sub>9</sub> H <sub>20</sub> )            | 128.2 | 14.9-18.3 |
| Decane: (C <sub>10</sub> H <sub>22</sub> )           | 142.3 | 18.0-27.9 |
| Undecane: (C <sub>11</sub> H <sub>24</sub> )         | 156.3 | 8.5-16.2  |
| Dodecane: (C <sub>12</sub> H <sub>26</sub> )         | 170.3 | 0.6-1.8   |
| Hexadecane: (C <sub>16</sub> H <sub>34</sub> )       | 226.4 | <0.10     |
| Benzene: (C <sub>6</sub> H <sub>6</sub> )            | 78.1  | 0.85-4.7  |
| Isopropylbenzene: (C <sub>9</sub> H <sub>12</sub> )  | 120.2 | 3.3-5.6   |
| Xylenes: (C <sub>8</sub> H <sub>10</sub> )           | 106.2 | 35.6-74.1 |
| Toluene: (C <sub>7</sub> H <sub>8</sub> )            | 92.1  | 4.96-37.2 |

|  |     |                          |
|--|-----|--------------------------|
| DimethylMercury (CH <sub>3</sub> ) <sub>2</sub> Hg | 231 | 2.1-91 ng/m <sup>3</sup> |
|--|-----|--------------------------|

# SULFUR REMOVAL PROCESSES



| Biogas | Contaminant      | Concentration          |                         |
|--------|------------------|------------------------|-------------------------|
| LFG    |                  | Highest                | Typical                 |
|        | H <sub>2</sub> S | 5400 ppmv              | 63 ppmv                 |
|        | Siloxanes        | 54 mg/Nm <sup>3</sup>  | 16.8 mg/Nm <sup>3</sup> |
| WWTP   | H <sub>2</sub> S | 3 %                    | 400 ppmv                |
|        | Siloxanes        | 400 mg/Nm <sup>3</sup> | 46 mg/Nm <sup>3</sup>   |

Figure 1: Hydrogen sulphide processing selection chart.



# SILOXANES (ACCELERATED TESTING)

| Sample       | Nomenclature | Theoretical<br>Mass gain SiO <sub>2</sub> | Actual Mass<br>Gain SiO <sub>2</sub> | % error |
|--------------|--------------|---|--------------------------------------|---------|
| 1 week NiMg  | 1W-NiMg      | 2.6%                                      | 1.5%                                 | -43.5%  |
| 1 month NiMg | 1M-NiMg      | 11.1%                                     | 11.9%                                | 7.5%    |
| 6 month NiMg | 6M-NiMg      | 66.7%                                     | 65.7%                                | -1.5%   |
| 1week Pt     | 1W-Pt        | 2.6%                                      | 1.1%                                 | -59.4%  |
| 1 month Pt   | 1M-Pt        | 11.1%                                     | 10.5%                                | -5.4%   |
| 6 month Pt   | 6M-Pt        | 66.7%                                     | 61.9%                                | -7.2%   |



Fresh Catalyst



6 month poisoned

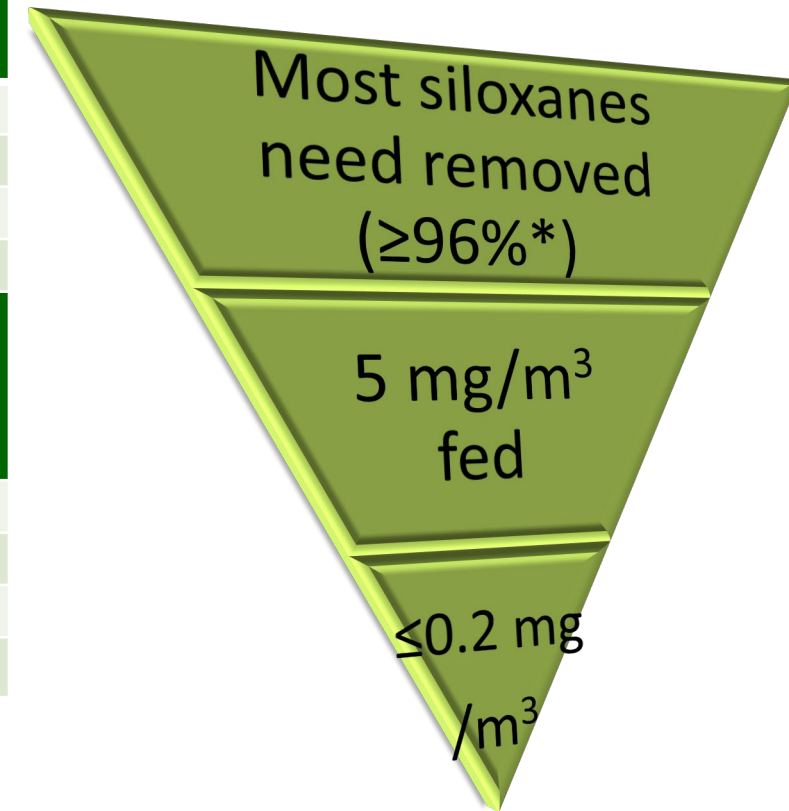
# SILOXANES (ACCELERATED TESTING)

| Pt Catalysts   | CH <sub>4</sub> Conversion Temperature (°C) |                 | CO <sub>2</sub> Conversion Temperature (°C) |                 | H <sub>2</sub> :CO (@450°C) |
|----------------|---|-----------------|---|-----------------|-----------------------------|
|                | X <sub>10</sub>                             | X <sub>50</sub> | X <sub>10</sub>                             | X <sub>50</sub> |                             |
| Fresh*         | 454   | 603             | 432   | 578             | 0.30                        |
| 1W-Pt          | 518   | 630             | 503   | 613             | 0.22                        |
| 1M-Pt          | 535   | 675             | 510   | 657             | 0.20                        |
| 6M-Pt          | 587   | 752             | 566   | 726             | 0.11                        |
| NiMg Catalysts | CH <sub>4</sub> Conversion Temperature (°C) |                 | CO <sub>2</sub> Conversion Temperature (°C) |                 | H <sub>2</sub> :CO (@800°C) |
|                | X <sub>10</sub>                             | X <sub>50</sub> | X <sub>10</sub>                             | X <sub>50</sub> |                             |
| Fresh          | 762   | 848             | 742   | 813             | 0.31                        |
| 1W-NiMg        | 810   | 900             | 790   | 875             | 0.13                        |
| 1M-NiMg        | 842   | nr              | 827   | 900             | 0.09                        |
| 6M-NiMg        | nr  | nr              | 900   | nr              | n/a                         |

Conversions for methane dry reforming

-nr: Not reached

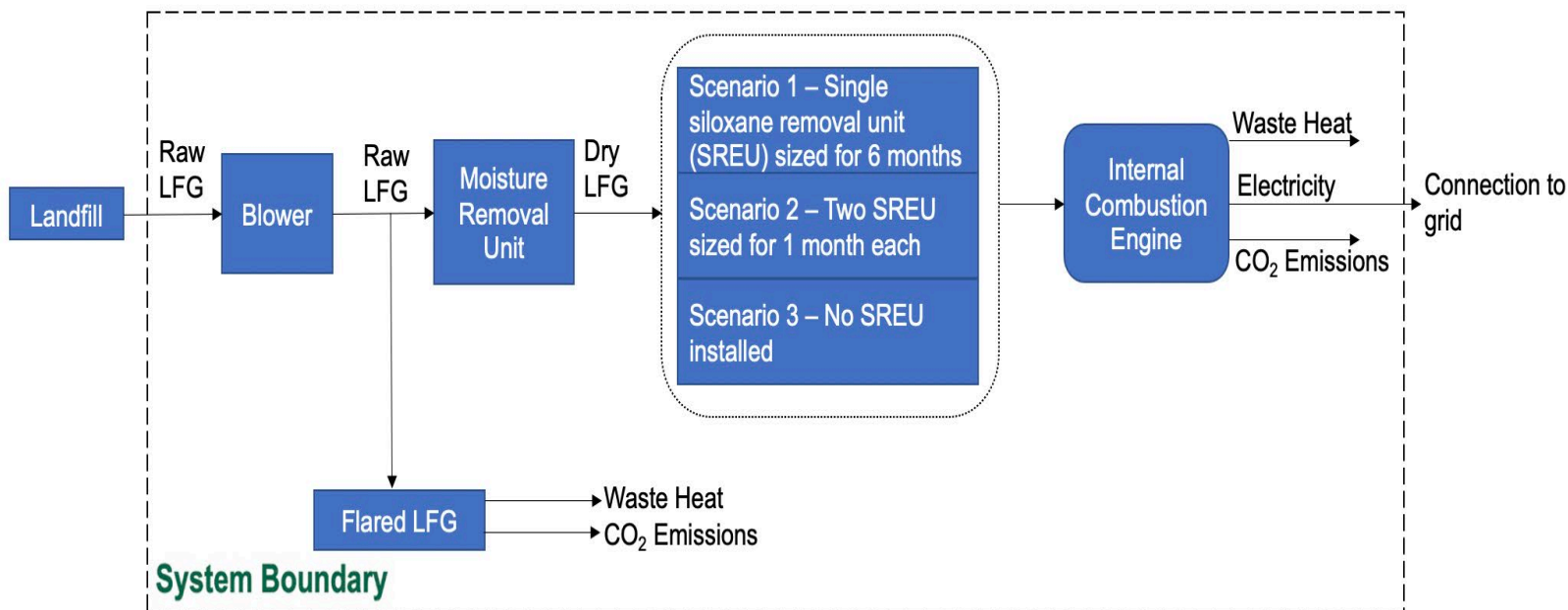
n/a: not applicable since there was no reactant conversion



\* Based on speculation that performance 1 week samples may be acceptable



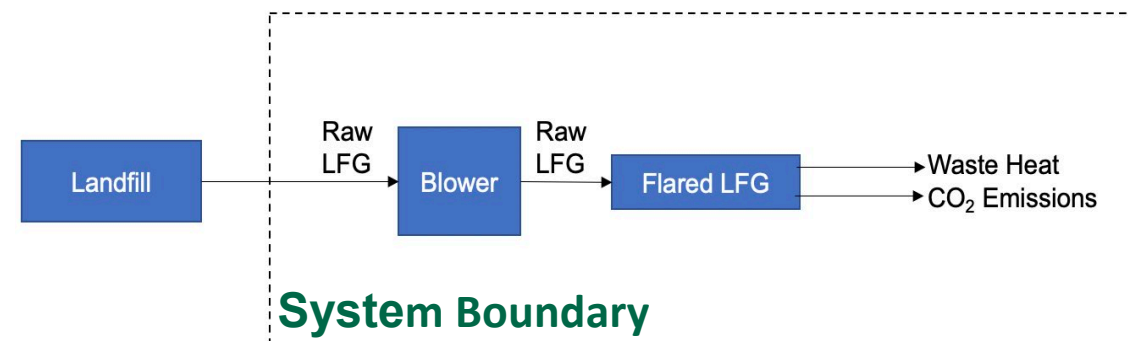
# SILOXANE REMOVAL FROM LFG



- Four Scenarios studied.
- 1<sup>st</sup>, 2<sup>nd</sup> and 3<sup>rd</sup> scenarios generated electricity.
- 4<sup>th</sup> scenario flared LFG.

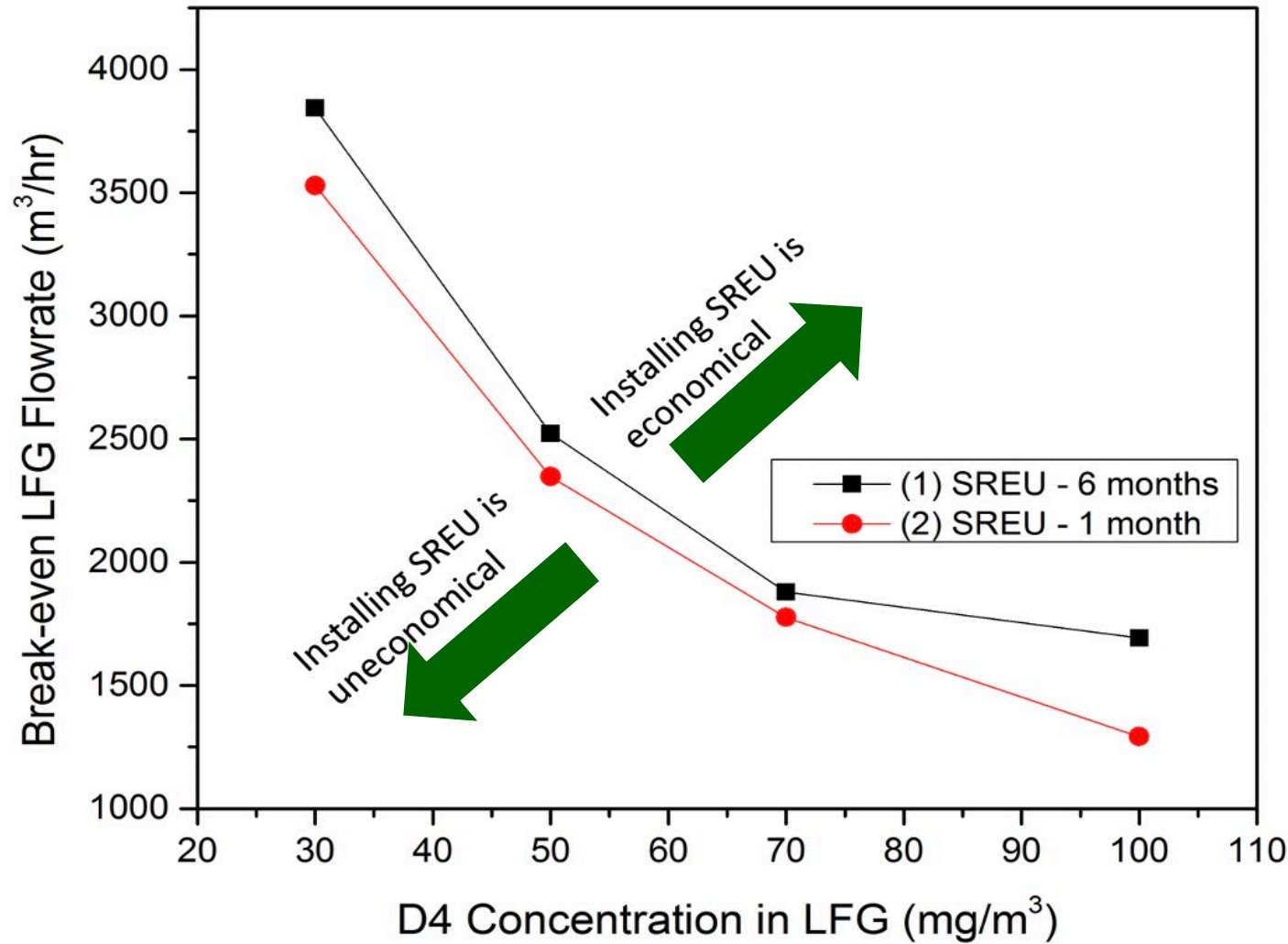
## Facilities that generates electricity (Scenarios 1 - 3)

- 1<sup>st</sup> and 2<sup>nd</sup> scenarios installed siloxane removal units.
- 3<sup>rd</sup> scenario did not install siloxane removal unit.



Facility that flares all LFG captured (Scenario 4).

# TEA RESULTS



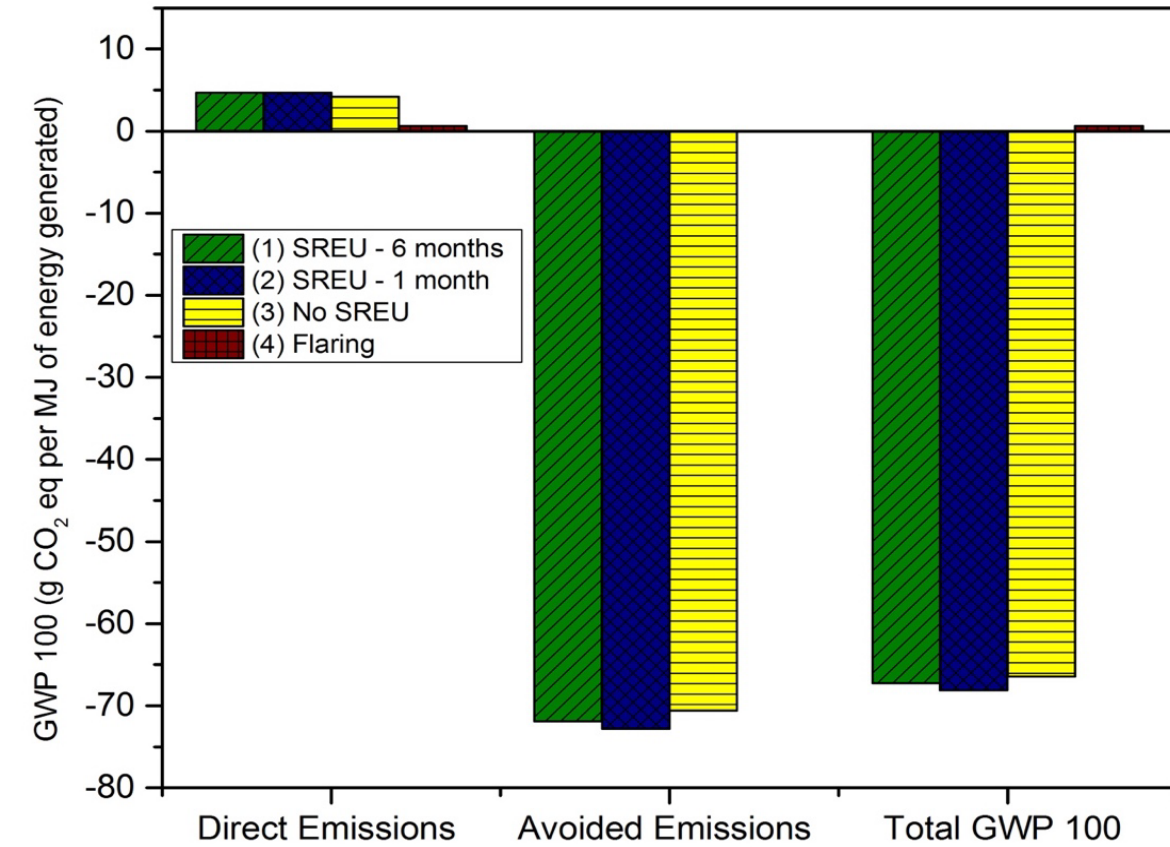
The figure shows the LFG flowrate at which it becomes economical to install a SREU as a function of siloxane concentration in LFG.

SREU – Siloxane Removal Unit.

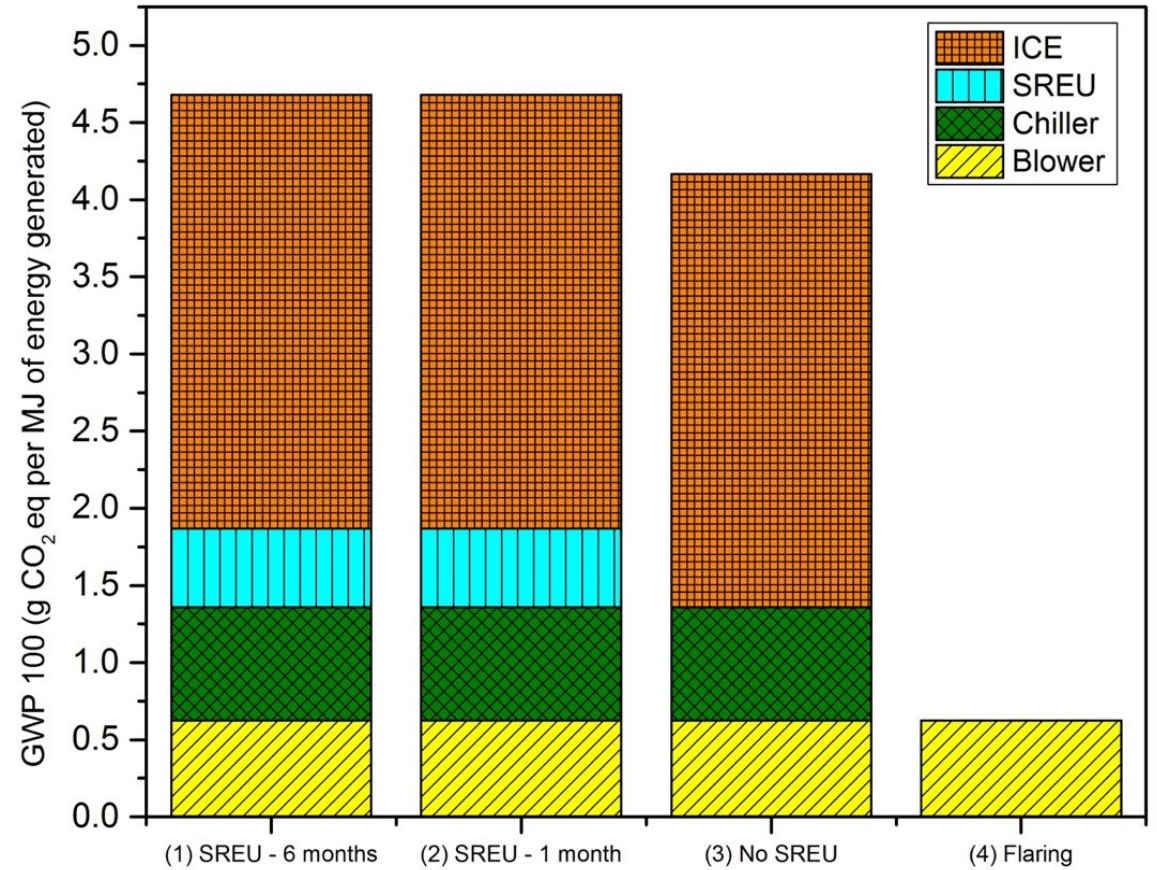
It is seen that as the siloxane concentration increases, the break-even LFG flowrate reduces.

Effect of D4 concentration and biogas flowrate on the annual net cash income.

# LCA Results



Comparison of Direct, Avoided and Total Emissions in terms of GWP 100 among the four scenarios (Base case: 1700 m<sup>3</sup>/hr. LFG (50% CH<sub>4</sub>), 50 mg/m<sup>3</sup> D<sub>4</sub>).

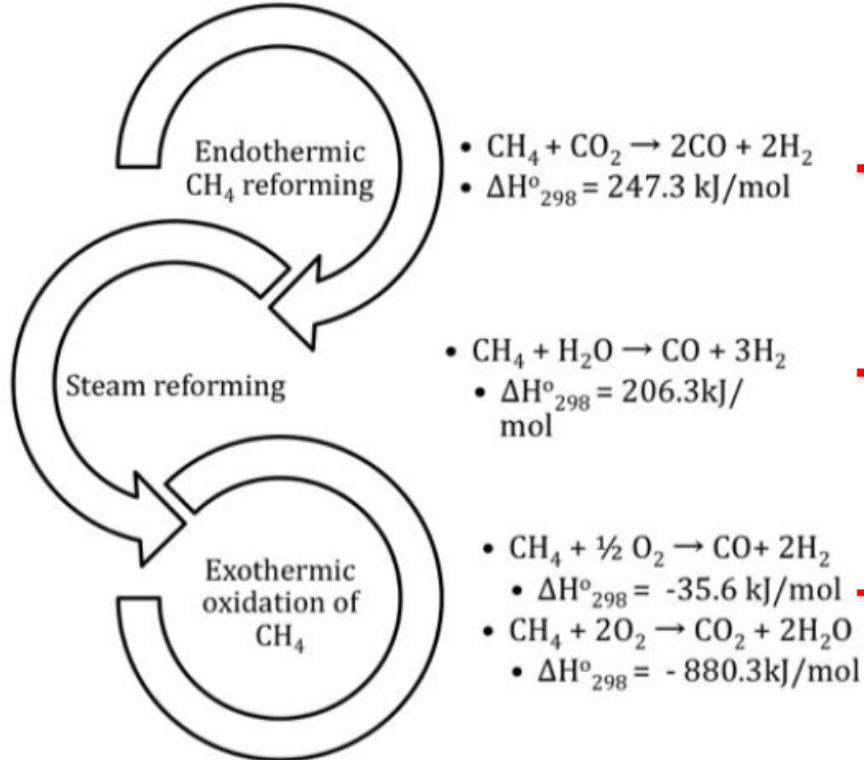
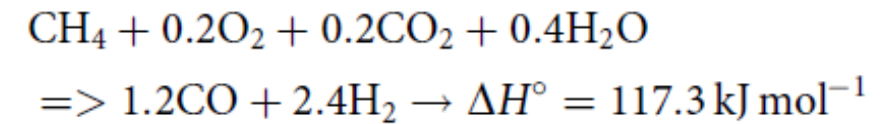


GWP 100 of the LFG blower/treatment system and ICE for the four scenarios (Base case: 1700 m<sup>3</sup>/hr. LFG (50% CH<sub>4</sub>), 50 mg/m<sup>3</sup> D<sub>4</sub>).

# CATALYTIC TRI-REFORMING

- Minimize cleanup and pretreatment process (No CO<sub>2</sub> removal)
- Less energy consumption
- Produce high quality syngas (H<sub>2</sub>:CO ~ 2)

Global reaction (within constraints)



**Utilize 100% of biogas as feedstock**

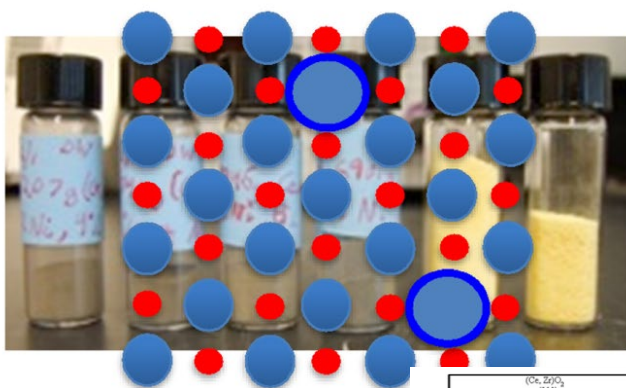
**Control H<sub>2</sub> and CO selectivity**

**Generate heat in-situ**

From our results, we estimate  $\Delta H_r$  (T=800°C) = 135 kJ/mol CH<sub>4</sub> X



# CATALYTIC TRI-REFORMING

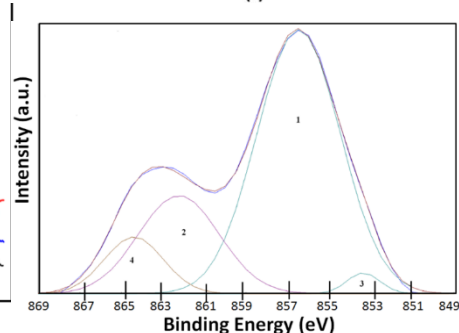
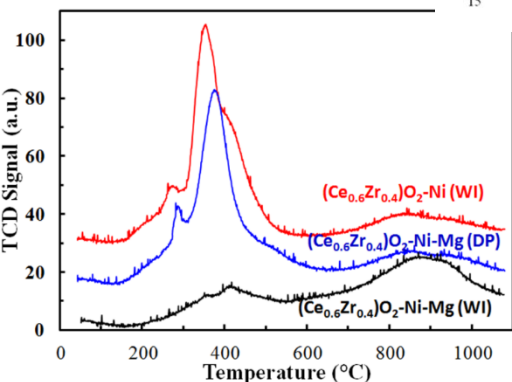
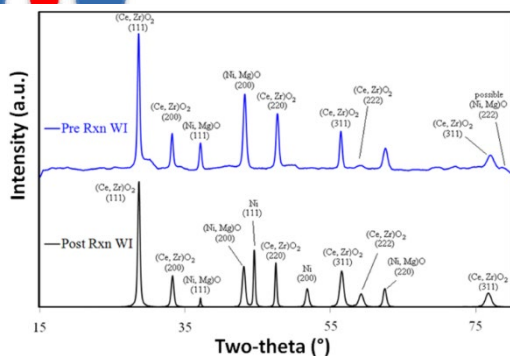
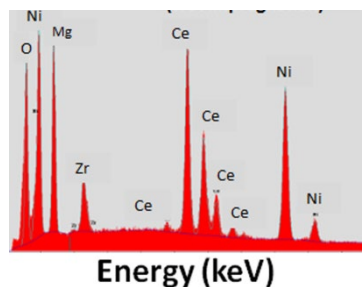


Ni-Mg-(Ce,Zr)O<sub>2</sub>  
catalysts \*

● = Zr (0.84Å)

● = Ce<sup>4+</sup> (0.97Å)

● = Ce<sup>3+</sup> (1.14Å)



**Tri-reforming of LFG** (LFG : air : H<sub>2</sub>O = 1.00 : 0.56 : 0.36)

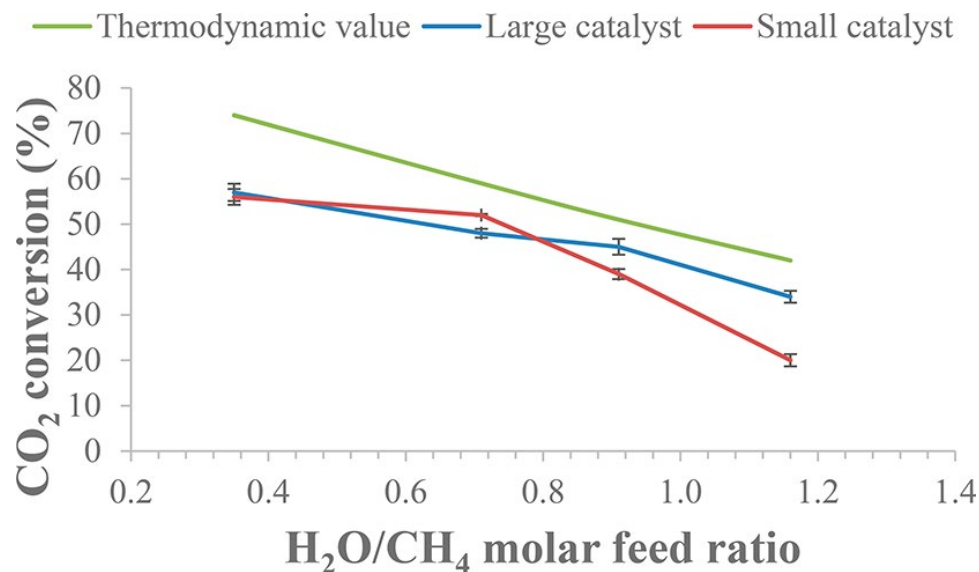
| Catalyst Bed temp. (°C) | GHSV (h <sup>-1</sup> ) | CH <sub>4</sub> conv. (%) | CO <sub>2</sub> conv. (%) | H <sub>2</sub> :CO |
|-------------------------|-------------------------|---------------------------|---------------------------|--------------------|
| 770-810                 | 30,000                  | 92-99                     | 52-72                     | 1.70-2.23          |

## Catalyst Optimization

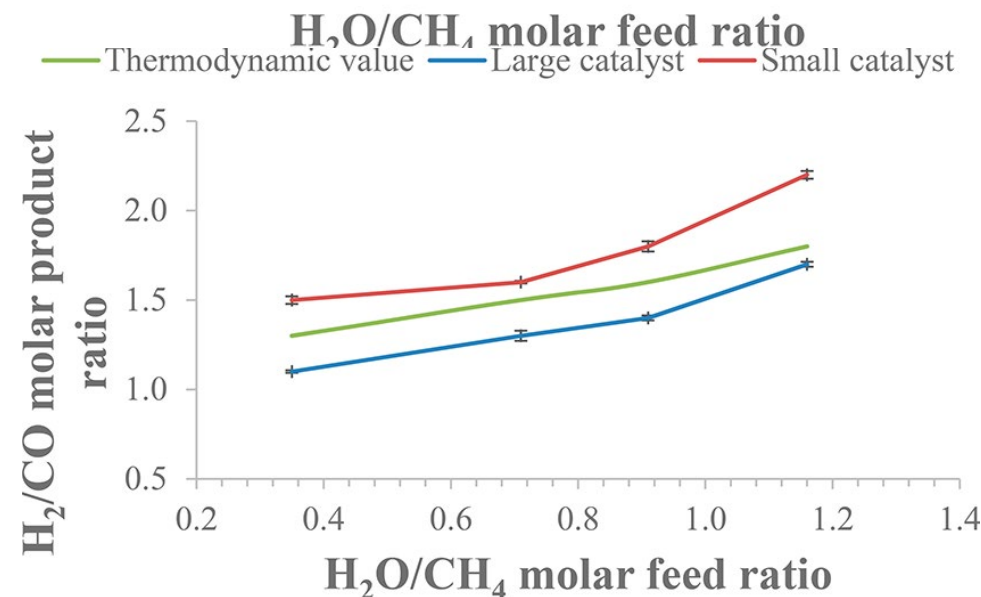
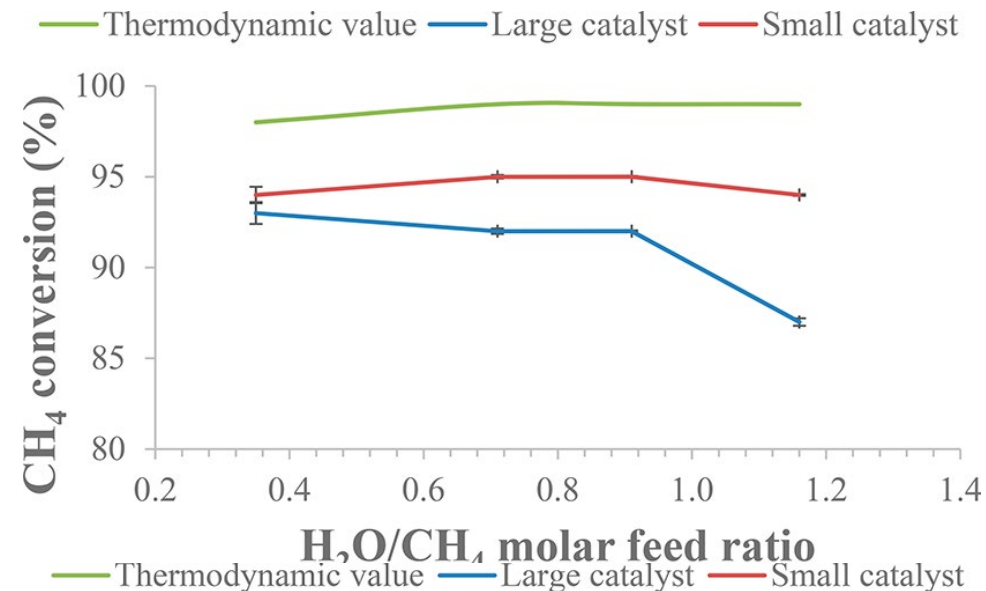
Thermally Stable  
High Surface Area  
Coke Resistant  
High OSC  
Excellent Redox Properties  
High Dispersion  
Excellent Selectivity  
High Activity  
Economical  
Low Pressure Drop



# COMPETITION OF CO<sub>2</sub> & H<sub>2</sub>O



- CO<sub>2</sub> X => 0 at 2:1 ratio
- Coking rate ~ 1E-4 g/g/hr



**Analysis of Internal Diffusion Limitations**

|   | internal diffusion limitation, $C_{wp}$ | Thiele modulus, $\Phi_n$ | effectiveness factor, $\eta$ | radius (mm) | length (mm) |
|---|---|--------------------------|------------------------------|-------------|-------------|
| large catalyst  | 38                                      | 6.2                      | 0.16                         | 1.59        | 7.0         |
| small catalyst  | 7                                       | 2.7                      | 0.37                         | 0.75        | 2.0         |
| NiMg/<br>Ce <sub>0.6</sub> Zr <sub>0.4</sub> O <sub>2</sub><br>powder | 0.12                                    | <1                       | 1.0                          | 0.06        | N/A         |



# REAL LFG

| Conditions   | Feed<br>(CH <sub>4</sub> :CO <sub>2</sub> :H <sub>2</sub> O:air by mole) | CH <sub>4</sub> X<br>(%) | CO <sub>2</sub> X<br>(%) | H <sub>2</sub> :CO ratio |
|--|--|--------------------------|--------------------------|--------------------------|
| *, 3 bar, ~30k h <sup>-1</sup>                           | LFG + air + steam*   | 92-99                    | 52-72                    | 1.7-2.2                  |
| 882 °C, 3 bar, ~26k h <sup>-1</sup>                      | 1: 0.7: 1.16: 0.95   | 87                       | 34                       | 1.7                      |
| Control: powder<br>(800 °C, 1 bar, 61k h <sup>-1</sup> ) | 1: 0.7: 0.23: 0.2 (O <sub>2</sub> )                                      | 97                       | 78                       | 2.1                      |



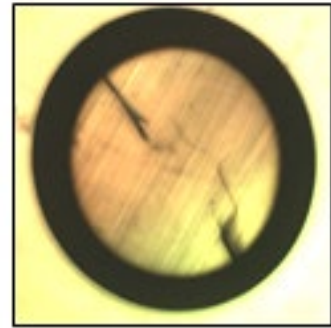
\* Temperature and steam added varied, LFG purified, raw LFG ~ 56% methane and 40% CO<sub>2</sub>

# CO-BASED FTS CATALYST

## FTS Eggshell Catalyst



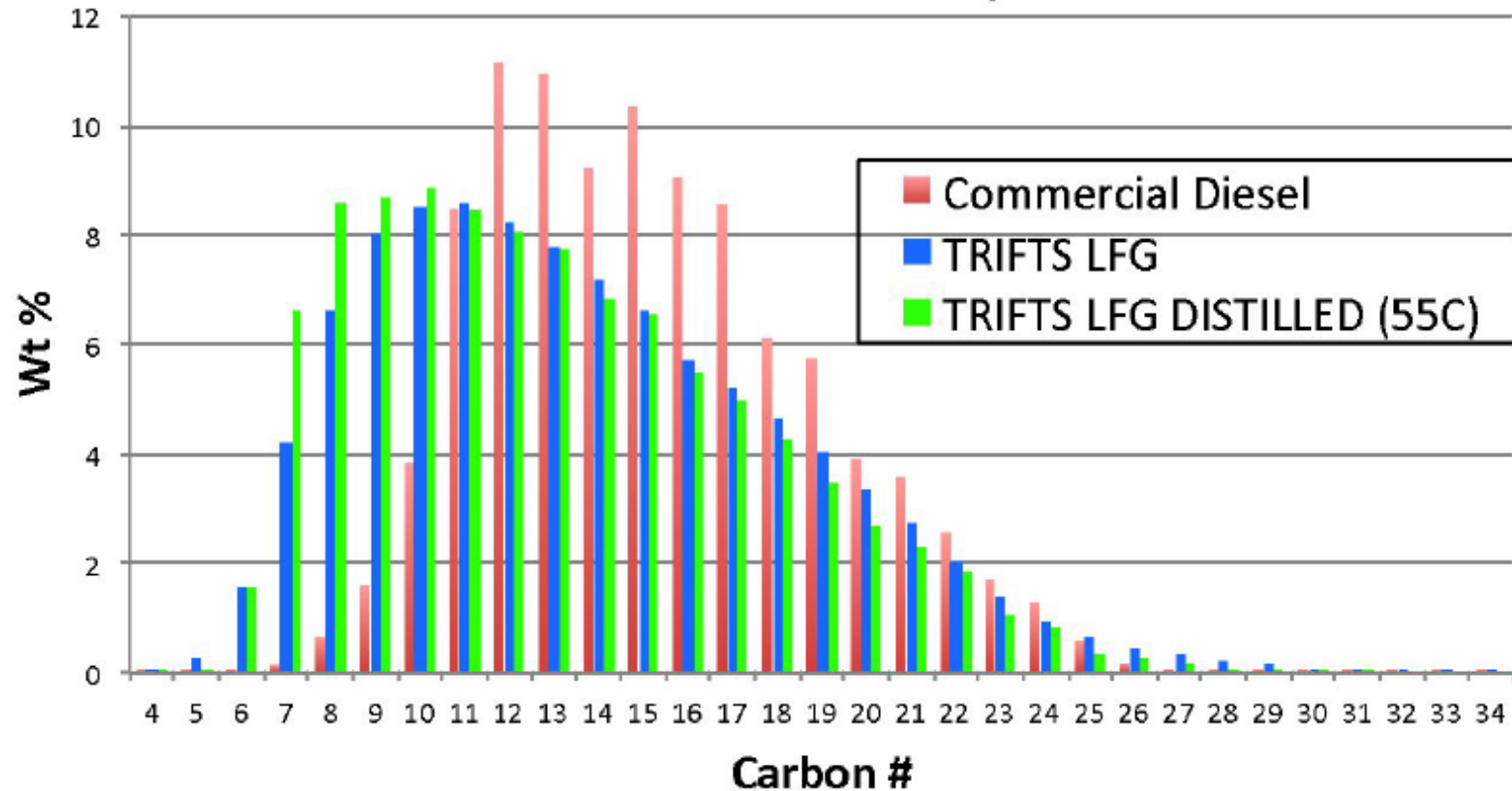
- Overcome mass and heat transfer limitations
- Selective product distribution in middle distillate region
- Avoid wax production



| CO % Conv | LFG Energy Recovery<br>In Liq Fuel (%) | Selectivity (%)  |                 |                 |
|-----------|--|------------------|-----------------|-----------------|
|           |  | C <sub>1-4</sub> | CO <sub>2</sub> | C <sub>5+</sub> |
| 71        | 40                                     | 43.7             | 1.4             | 55.0            |

# FUEL ANALYSIS

- Low aromatics improve net heat of combustion and reduce soot
- Isomers improve cold temp properties
- Further reduce olefin content w/ addition of catalyst promoters
- Excellent middle distillate boiling point distribution
- Control phase separation temp to fractionate light ends
- Final boiling point aligns with commercial diesel



| HC Family/Diesel | TriFTS | Commercial |
|------------------|--------|------------|
| P – I – O        | 99.7%  | 53%        |
| Cyclics (+A)     | 0.3%   | 47%        |

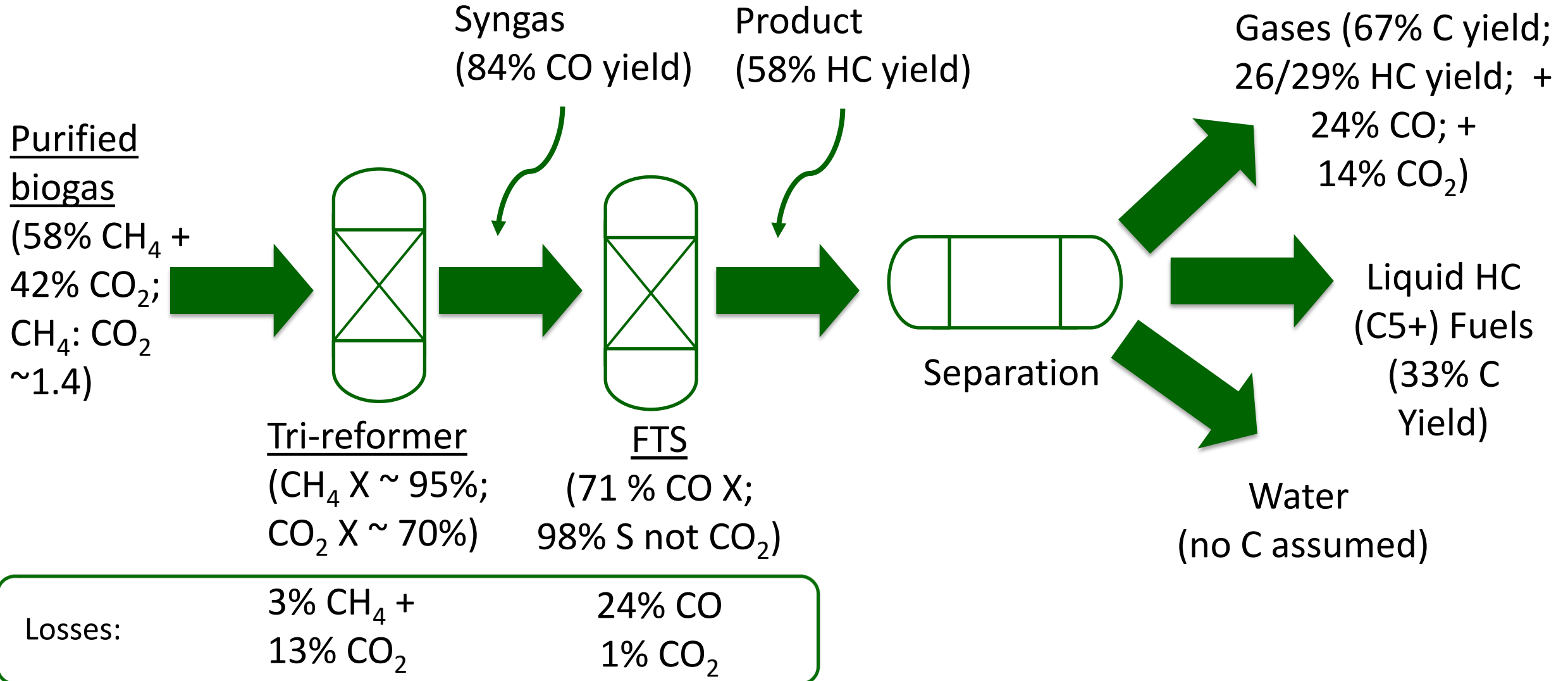
# FUEL ANALYSIS

## ASTM D975 “Standard Specification for Diesel Fuel Oils”

### Fuel Analysis Results

| Fuel Analysis, ASTM Standard        | Spec (No. 2 Diesel) | Commercial Diesel | TRIFTS LFG | TRIFTS LFG (Dist 55C) |
|-------------------------------------|---------------------|-------------------|------------|-----------------------|
| Specific Gravity, ASTM D4052 (g/cc) |                     | 0.8215            | 0.7386     | 0.7489                |
| Cetane Index, ASTM D976             | ≥ 40                | 57.6              | 84.5       | 72.7                  |
| Cetane Index, ASTM D4737            | ≥ 40                | 59.7              | 92.3       | 83.4                  |
| Flash Point, ASTM D93 (°C)          | ≥ 52                | 87                | 49         | 57                    |
| Cloud Point, ASTM D2500 (°C)        |                     | -6                | -6         | -3                    |
| Pour Point, ASTM D97 (°C)           |                     | -9                | -9         | -6                    |
| Distillation, ASTM D86 (°C)         |                     |                   |            |                       |
| IBP: 0.5wt%                         |                     | 203               | 143        | 142                   |
| 10%                                 |                     | 220               | 164        | 154                   |
| 50%                                 |                     | 269               | 234        | 216                   |
| 90%                                 | 282-338             | 329               | 327        | 314                   |
| FBP: 99.5%                          |                     | 378               | 388        | 378                   |
| Net Heat Comb., ASTM D3338 (MJ/kg)  |                     | 43.164            | 44.520     | 44.355                |

# TRIFTS PROCESS OVERVIEW\*



\* Neglecting purification train here (material losses minimal; energy losses vary)



# PILOT SCALE (THE DREAM ~ 2013)

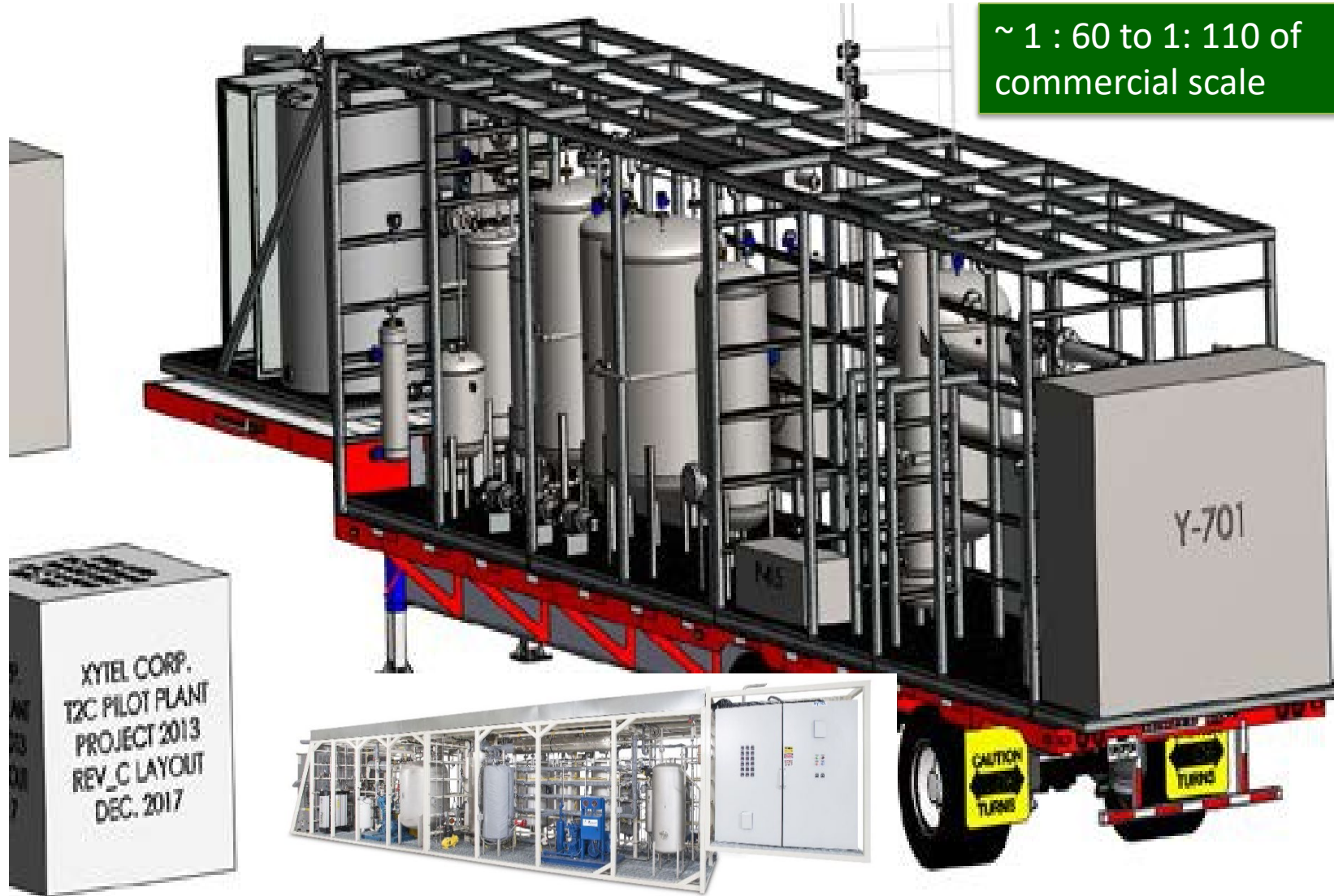


(24 scfm feed → 75 gal/day diesel)



# PILOT SCALE (THE PLAN 2017-18)

~ 1 : 60 to 1 : 110 of  
commercial scale





# PILOT SCALE (THE FIRST TEST SITE 2019)





# PILOT SCALE (CITRUS COUNTY 2019-20)



DOE site visit  
“verification”  
Feb. 2020





# PILOT SCALE (PINELLAS COUNTY 2021)

**South Cross Bayou Advanced Water  
Reclamation Facility (AWRF): *Environmental  
Commitment through Resource Recovery***



Image:  
<https://www.pinellascounty.org/utilities/south-cross.htm>

First biogas from WWTP test  
Oct. 2021



# MAJOR DOE MILESTONE: 2022

## Department of Energy's Bioenergy Office Achieves Major Biofuel Technology and Production Milestone

JULY 26, 2022



[Bioenergy Technologies Office »](#)

### Department of Energy's Bioenergy Office Achieves Major Biofuel Technology and Production Milestone



Author: Josh Messner,  
Technology Manager, Systems

The U.S. Department of Energy Bioenergy Technologies Office (BETO) has achieved a significant milestone in decreasing the minimum fuel selling price (MFSP) of drop-in biofuels, which are fuels made from biomass and other waste carbon sources, and that are compatible with existing petroleum fuel infrastructure and conventional vehicles. BETO partnered with T2C-Energy, LLC (T2C) to validate pilot-scale production of drop-in biofuels with a price of \$3 per gallon of gas equivalent (GGE) and at least 60% lower greenhouse gas emissions than petroleum, using T2C's TRIFTS<sup>®</sup> process.



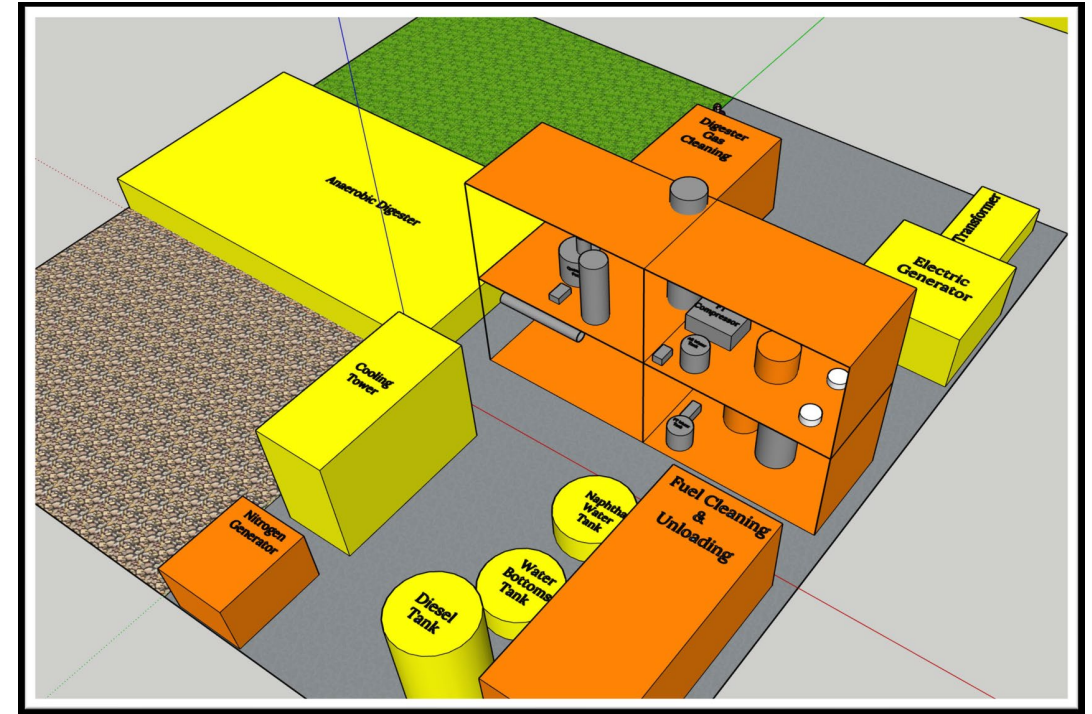
# WHAT'S NEXT?! 2 DOE AWARDS FOR FULL SCALE

**Project Title: Demonstration Scale-up: TRIFTS Biogas to Renewable Fuel**

**Lead Organization: T2C-Energy, LLC**

**Principal Investigator: Devin Walker**

T2C-Energy developed and patented a proprietary process, we have trademarked TRIFTS®, by which to convert biogas (or landfill gas) to liquid transportation fuels. This project seeks to scale the TRIFTS technology to enable the design and construction of a demonstration plant achieving a TRL of 7 by the end of the project. The TRIFTS process has been thoroughly tested at the pilot scale (over the past two years) processing a 9-24 scfm slipstream of raw biogas into drop-in renewable transport fuel. The process is capable of utilizing both the carbon dioxide and methane portions of biogas and incorporates the biogenic carbon from them into the hydrocarbon backbone of the final fuel product of the process. In doing so the technology essential uses 100% of the biogas as a feedstock. The use of carbon dioxide (CO<sub>2</sub>) is a critical cost reduction step as it represents 40-50% of the total makeup of biogas effectively doubling the utilizable carbon compared to technologies that remove CO<sub>2</sub> utilizing expensive pretreatment processes. We have previously identified a candidate landfill with our project partners to implement a 1,300 scfm biogas capacity plant and produce over 1,000,000 gal/yr of renewable cellulosic diesel. This renewable source of diesel resembles its petroleum counterpart both physically and chemically, passing ASTM D975 specifications, and can be used in current



**Project Title:** TRIFTS Biogas to Renewable Fuel Technology Evaluation

**Project Applicant:** Yolo County

**Project Director/Principal Investigator:** Ramin Yazdani

**Project Investigators:** Mr. Devin Walker (T2C-Energy), Dr. Troy Hawkins (Argonne National Lab), Professor Anthony Wexler (UC Davis-Air Quality Research Center)

The Yolo County Department of Community Services, Division of Integrated Waste Management is applying to evaluate the Tri-reforming and Fischer Tropsch Synthesis

(trademarked TRIFTS®) Biogas to Renewable Fuel Technology. This project seeks to perform feasibility and technical demonstration testing to determine the best strategy to convert waste gas to energy at the Yolo County Central Landfill (YCCL). The main objective of this project is to

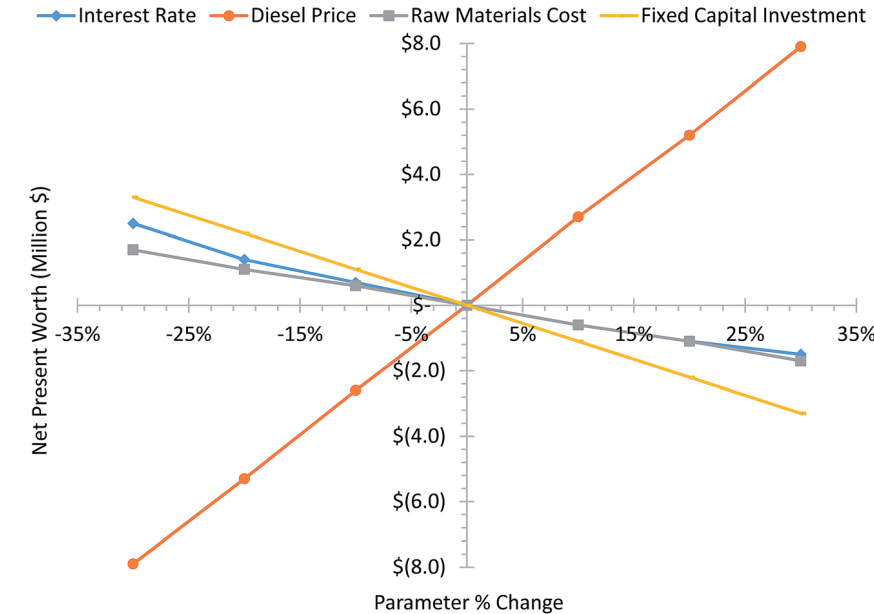


# PROCESS ECONOMICS

| Scale (LFG Flowrate SCFM) | CAPEX     | Annual OPEX | Annual Revenue | Annual Profit |
|---------------------------|-----------|-------------|----------------|---------------|
| 500                       | \$3.5 MM  | \$550 k     | \$3.5 MM       | \$2.1 MM      |
| 1000                      | \$5.2 MM  | \$800 k     | \$7 MM         | \$4.5 MM      |
| 1500                      | \$6.7 MM  | \$1 MM      | \$10.5 MM      | \$7.0 MM      |
| 2000                      | \$7.9 MM  | \$1.2 MM    | \$14 MM        | \$9.5 MM      |
| 2500                      | \$9.1 MM  | \$1.4 MM    | \$17.5 MM      | \$11 MM       |
| 3000                      | \$10.1 MM | \$1.6 MM    | \$21 MM        | \$14 MM       |
| 3500                      | \$11 MM   | \$1.8 MM    | \$24.5 MM      | \$16.8 MM     |
| 4000                      | \$11.9 MM | \$2 MM      | \$28 MM        | \$19 MM       |

## Assumptions

- 15% Interest Rate
- 35% Corporate Tax
- 5.5% FCI Maintenance Budget
- 7 Full Time Staff
- Wholesale Pump Price = \$1.63
- RIN = \$4.47/gal diesel (D3 ~ \$2.63/RIN) EV=1.7



Sensitivity analysis results. Base case is based on 15% interest rate, \$3.24 per gal diesel price, \$2.09 per MMBtu for LFG cost and total FCI of \$8.5 million.

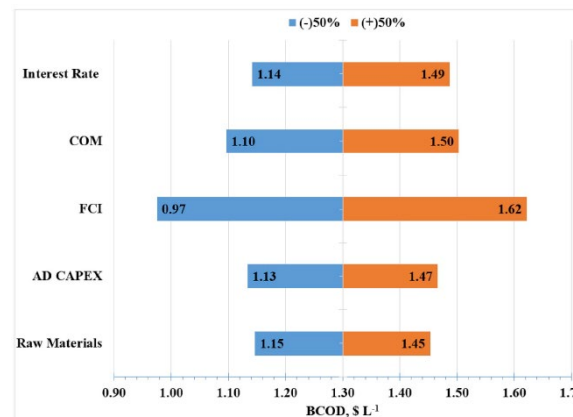
- Breakeven No RIN credit at 900 SCFM biogas production rate

# PROCESS ECONOMICS

Effect of tipping fee on feedstock on BCOD and NPW.

| Tipping Fee (\$<br>tonne <sup>-1</sup> ) | Feedstock Cost (\$<br>tonne <sup>-1</sup> ) | BCOD (\$<br>L <sup>-1</sup> ) | NPW (Million<br>\$) |
|--|---|-------------------------------|---------------------|
| 0  | 55  | 1.57                          | -10.9               |
| <b>0 (base case)</b>                     | <b>28</b>                                   | <b>1.30</b>                   | <b>0.00</b>         |
| 0  | 0   | 1.02                          | 10.9                |
| 28                                       | 0   | 0.80                          | 19.7                |
| 55                                       | 0   | 0.58                          | 28.6                |
| 83                                       | 0   | 0.36                          | 37.4                |

This Includes AD  
(~doubles the CAP-EX)



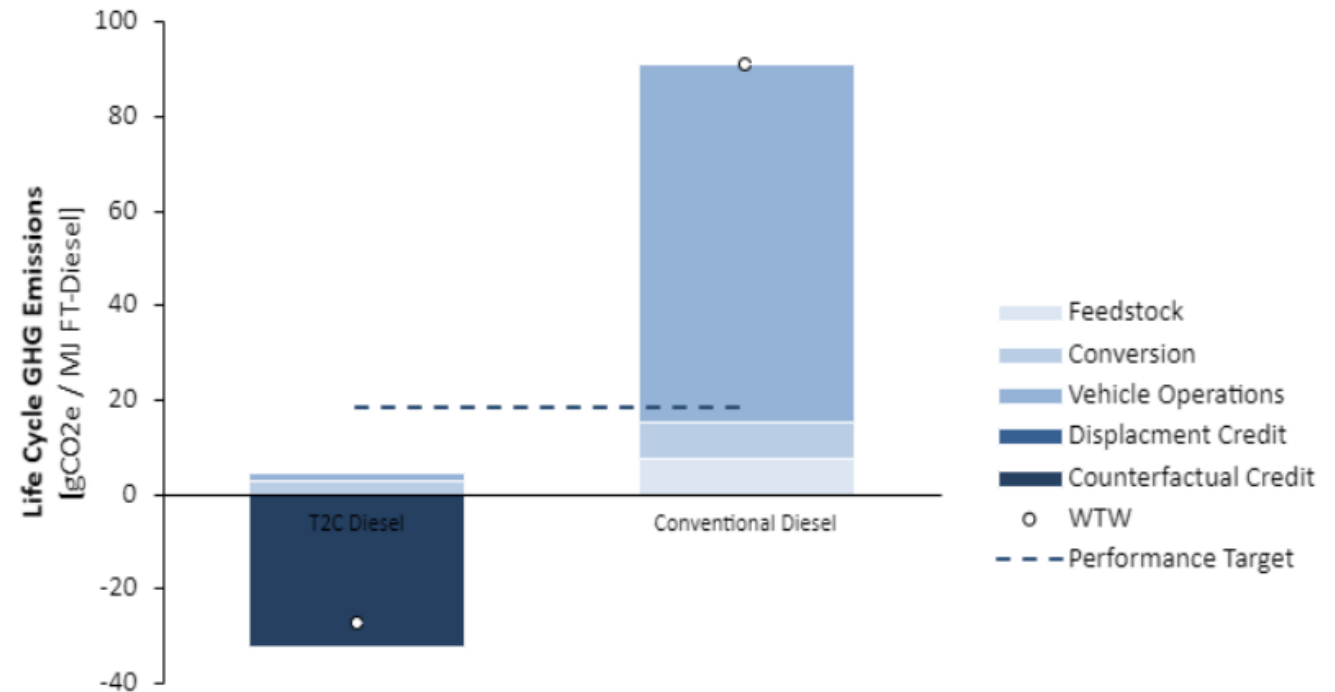
Economic comparison with published BTL modelling studies [72–74].

| BTL Techno-economic Study                                  | Interest on Capital Investment | Biomass Feed Capacity (dry tonne day <sup>-1</sup> ) | Production Cost of Diesel (\$ L <sup>-1</sup> ) |
|--|--------------------------------|--|---|
| Gasification-FT synthesis [72]                             | 10%                            | 2,016  | 0.56  |
| AD-BGTL  | 15%                            | 186  | 1.20  |
| Gasification-FT synthesis [73]                             | 10%                            | 1,920  | 0.73  |
| Gasification-FT synthesis followed by hydroprocessing [74] | 10%                            | 2,000  | 1.19  |

# ENVIRONMENTAL IMPACT

- HYSIS fully integrated with heat and mass recycle
- Biogas composition impacts (reactant feed auto tuning)
- ANL GREET model updated with TRIFTS Life Cycle Analysis
- Basic engineering design package (Global Docs completed)
  - Heat and mass balances
  - PFD's
  - General arrangement
  - P&ID's
  - Equipment / Instrument spec list
  - Control architecture
  - Pipe sizing and metallurgy study
- Engineering package Issued for Bids

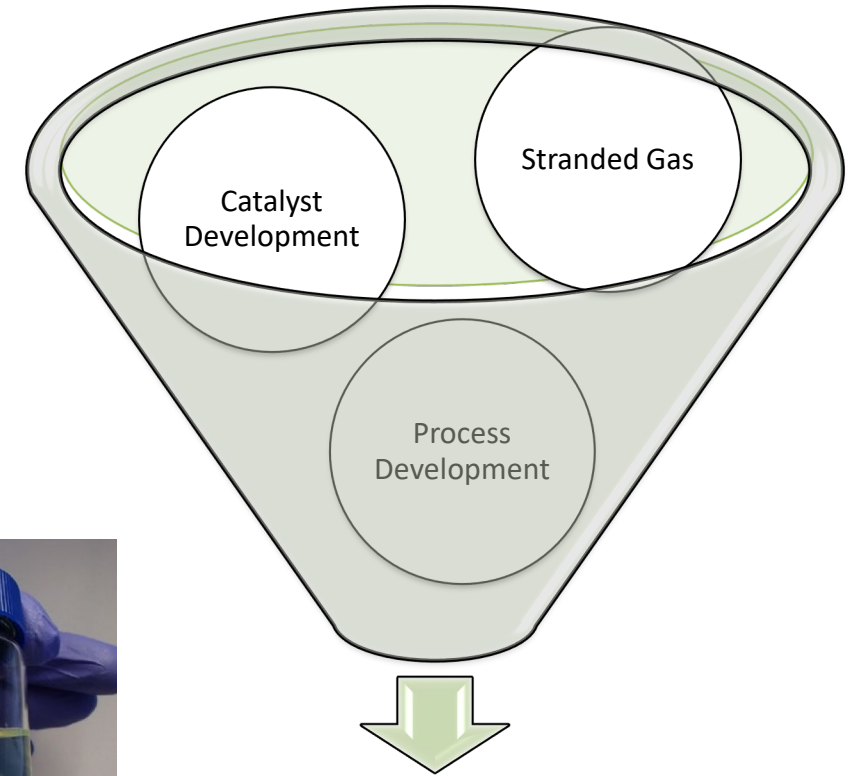
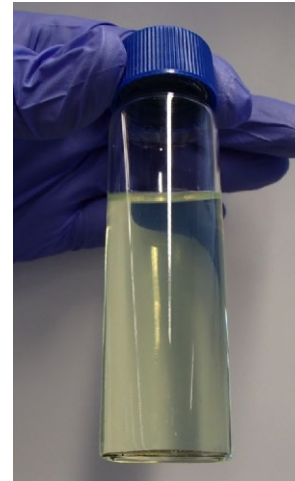
## ANL GREET Model Carbon Intensity Score



Landfill Application CI ~ - 36gCO<sub>2</sub>e/MJ

# SUMMARY

- Utilize most of Biogas Feedstock (CO<sub>2</sub> Utilization)
- Significant Reduction of Unit Operations
- Compatible with Current Infrastructure
- High Quality Value Added Product (Drop-In Diesel)
- Self Sufficient Process
- Produce D3/D7 RIN
- Vastly Improved Economics and Profitability, even in face of economies of scale

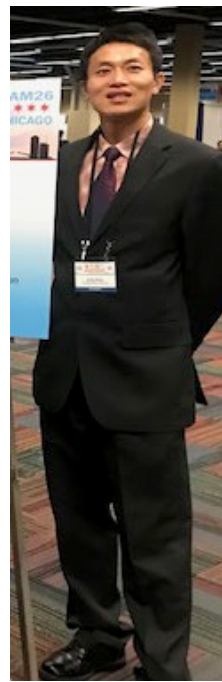
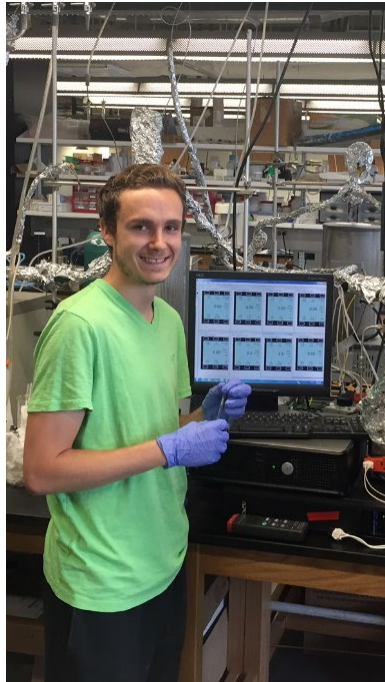
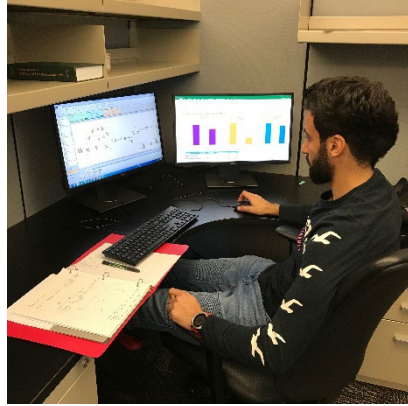


Viable Drop-in Fuels

~ 40% Energy &  
Carbon recovery



# THE TEAM



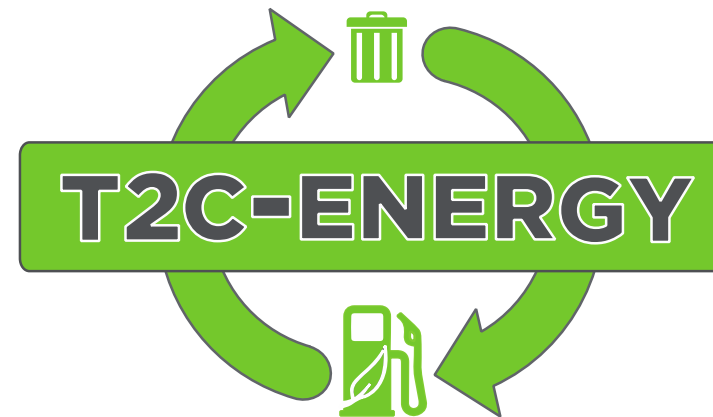
# Technologies for Upgrading Landfill Gas to a High-Quality Fuel

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John N. Kuhn

USF and T2C-Energy LLC

2023 SWANA FL Summer  
Conference

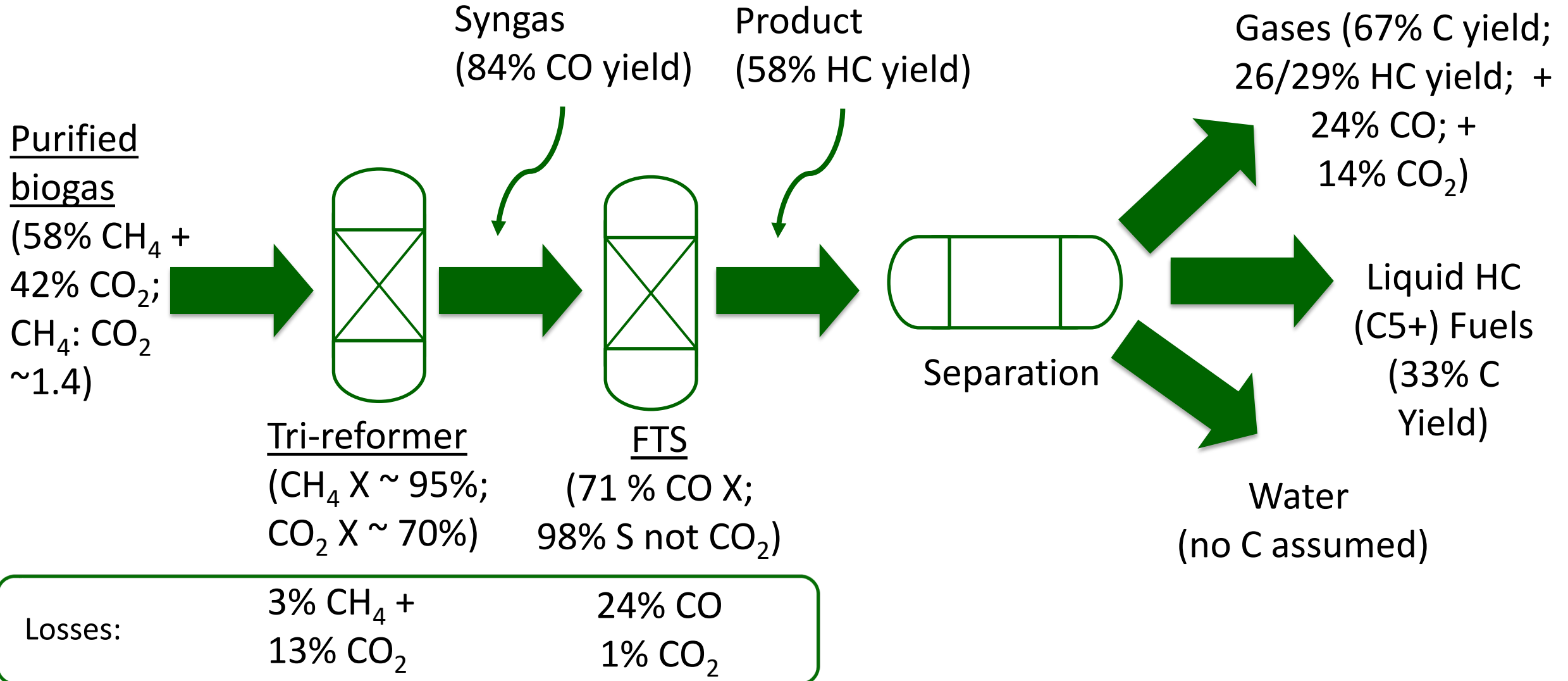


UNIVERSITY of  
**SOUTH  
FLORIDA**

# PARKED

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# TRIFTS PROCESS OVERVIEW\*



\* Neglecting purification train here (material losses minimal; energy losses vary)



# OVERALL M&EBs

